

Nº 179341

Fragilização por hidrogênio em pipelines

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PROIBIDO REPRODUÇÃO

Fragilização por hidrogênio em pipelines



Motivação

- Necessidade de transmissão de gás hidrogênio por longas distâncias
- Risco associado: fragilização

With the emergence of the new hydrogen economy and infrastructure, it is believed that piping and pipeline systems will need to be operated at pressures with possible cyclic pressure loading in excess of our current operating regimes. It is expected that hydrogen piping systems will have to be operated up to 100 MPa (15,000 psig), transport pipelines will operate up to 20 MPa (3,000 psig), and both piping and pipeline systems will be operating at or below 150°C (300°F). In doing so, the metallic pipe materials in use today could be placed in an operating environment for which we currently have little or no data on their mechanical properties and behavior in a dry hydrogen environment.

ASME B31.12

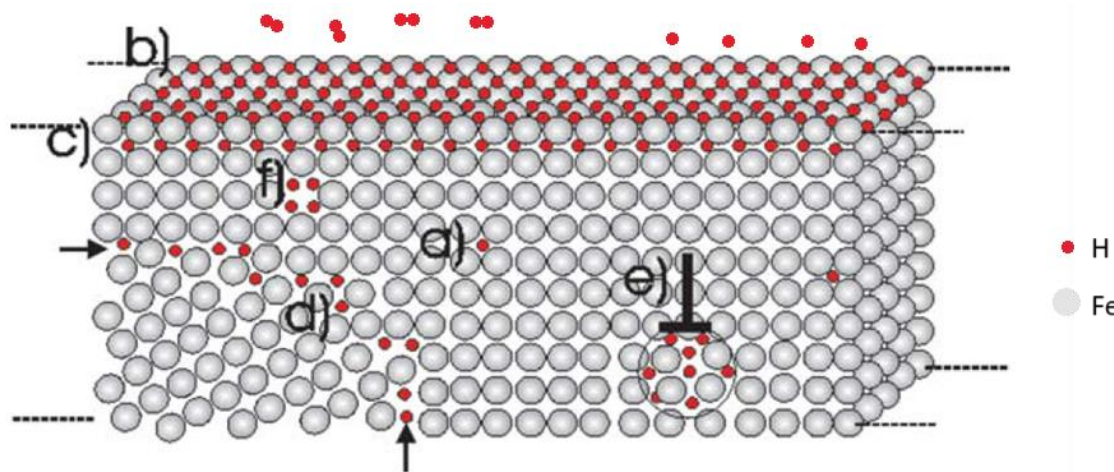
Danos por hidrogênio

- **Fragilização por hidrogênio (*hydrogen embrittlement* – HE)**
- **Trincamento devido à precipitação de hidrogênio (*hydrogen-induced cracking* – HIC)**
- ***Blistering***
- **Ataque por hidrogênio em alta temperatura (*high temperature hydrogen attack* – HTHA)**
- **Trincamento devido à precipitação de hidretos**

Danos por hidrogênio

- **Fragilização (*hydrogen embrittlement* – HE)**

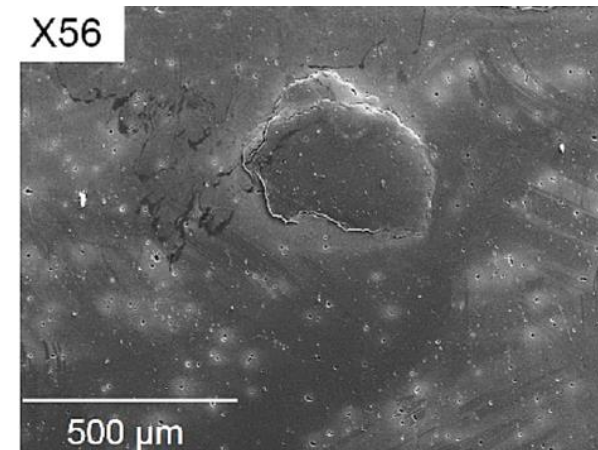
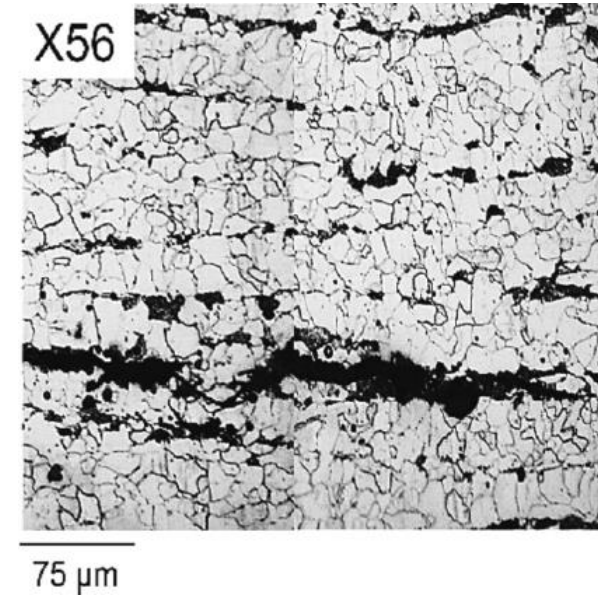
- Queda de ductilidade e tenacidade devido à presença de hidrogênio dissolvido, H (até 5 ppm)
- Alteração do mecanismo de fratura
- ↑ Resistência do material ↑ Susceptibilidade
- Reversível



Fonte: adaptado de <https://doi.org/10.1146/annurev.matsci.36.090804.094451>

Danos por hidrogênio

- Trincamento devido à precipitação de hidrogênio (*hydrogen-induced cracking – HIC*)
- Blistering
 - Manifestações do mesmo dano; propagação de trinca pela precipitação de hidrogênio molecular
 - Irreversível



Fonte: <https://doi.org/10.1016/j.engfailanal.2023.107650>.

Códigos/guias para pipelines transportando hidrogênio

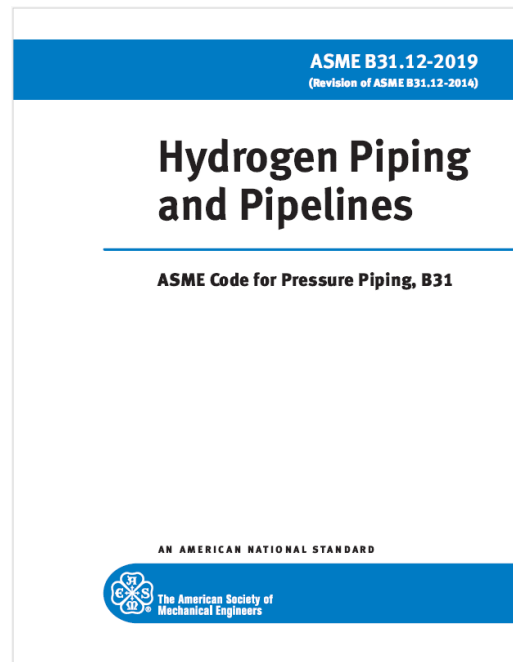


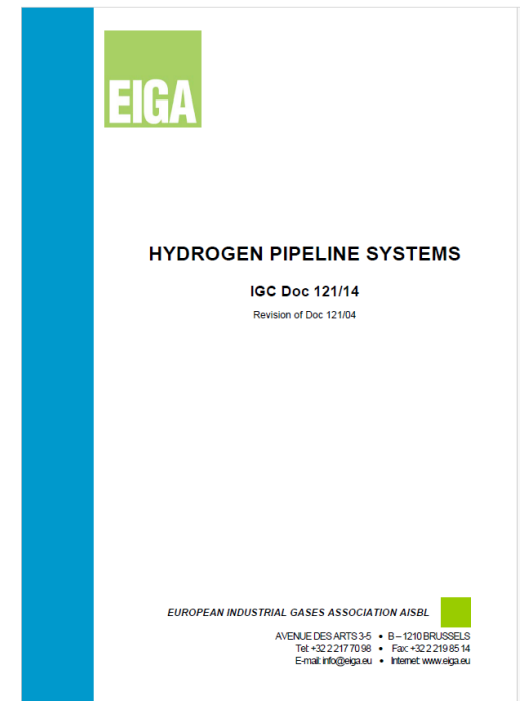
Table IX-5A
Carbon Steel Pipeline Materials Performance Factor, H_f

Specified Min. Strength, ksi		System Design Pressure, psig						
Tensile	Yield	≤1,000	2,000	2,200	2,400	2,600	2,800	3,000
66 and under	≤52	1.0	1.0	0.954	0.910	0.880	0.840	0.780
Over 66 through 75	≤60	0.874	0.874	0.834	0.796	0.770	0.734	0.682
Over 75 through 82	≤70	0.776	0.776	0.742	0.706	0.684	0.652	0.606
Over 82 through 90	≤80	0.694	0.694	0.662	0.632	0.610	0.584	0.542

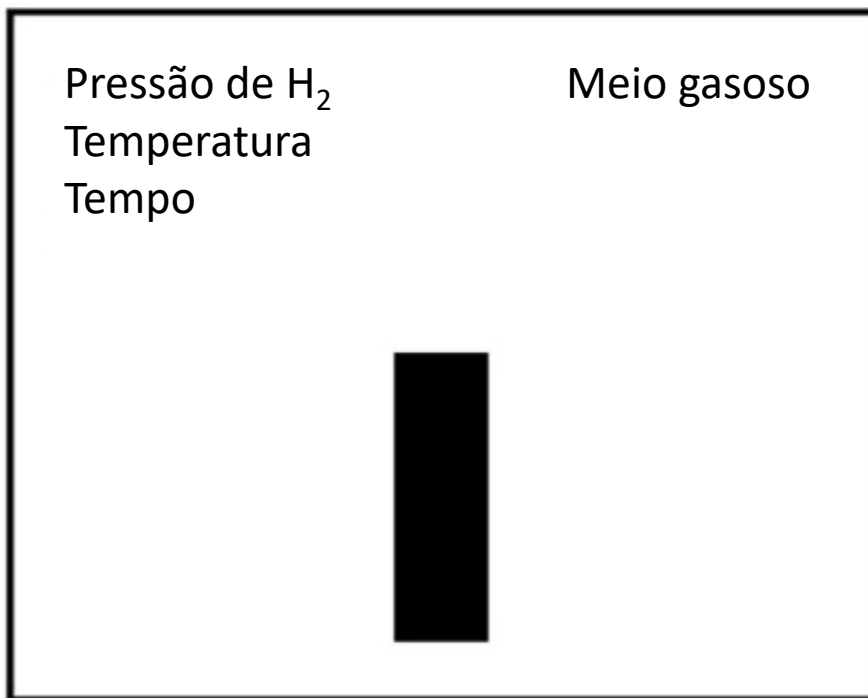
GENERAL NOTES:

- (a) Tables IX-5A, IX-5B, and IX-5C are for use in designing carbon steel, low, and intermediate alloy piping and pipeline systems that will have a design temperature within the hydrogen embrittlement range of the selected material [recommended lowest service temperature up to 300°F (150°C)]. If the system design temperature is out of this range, use the design allowable stresses from Table IX-1A for piping or the specified minimum yield strength for pipelines from Table IX-1B.
- (b) Table IX-5A was developed for pipeline systems and as such the design factors are based on the specified minimum yield strength of the material ranges shown.
- (c) Design factors may be calculated by interpolation between pressures shown in the tables.
- (d) For materials not covered by Tables IX-5A, IX-5B, and IX-5C, use the allowable stresses in Table IX-1A.

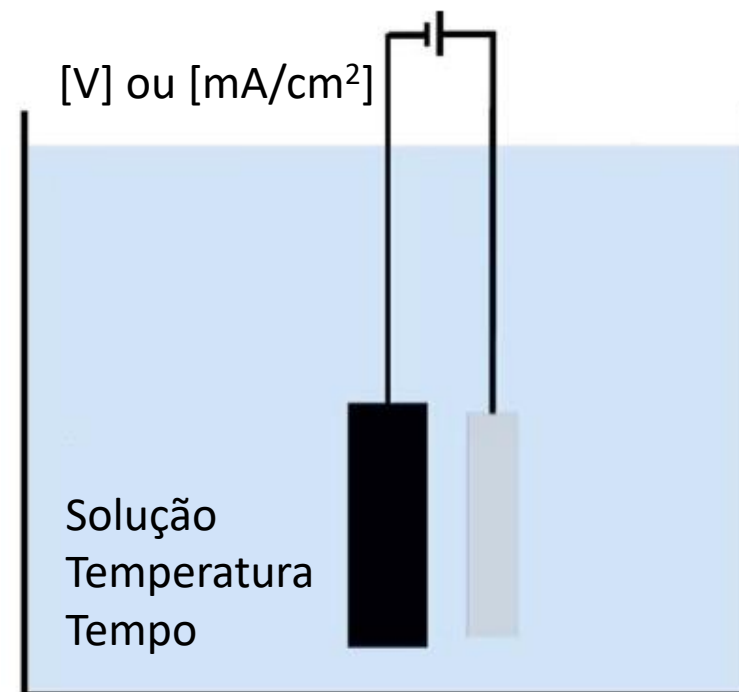
Classe de resistência máxima recomendada: X52



Literatura

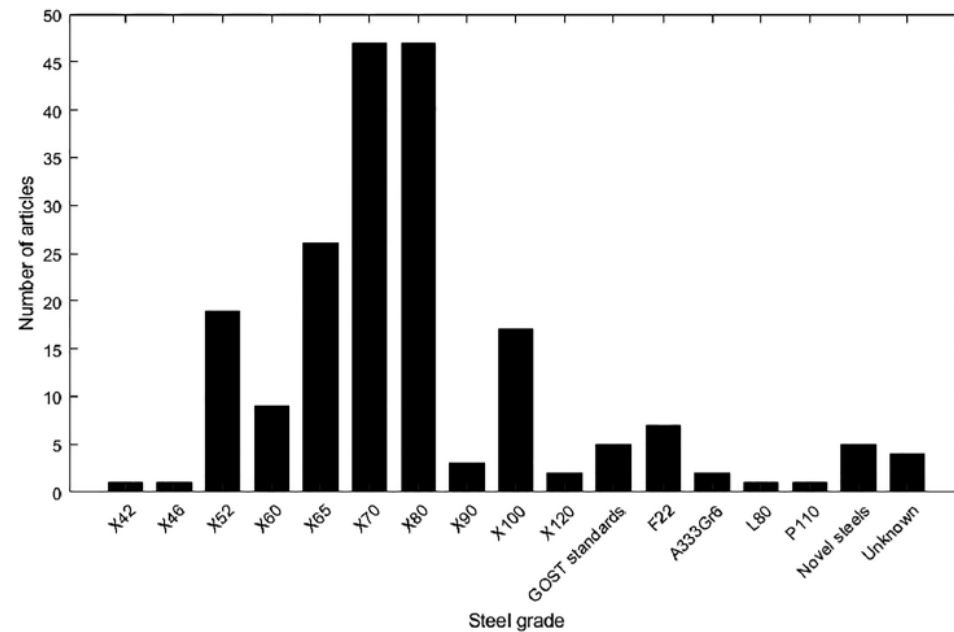


Carregamento gasoso



Carregamento catódico

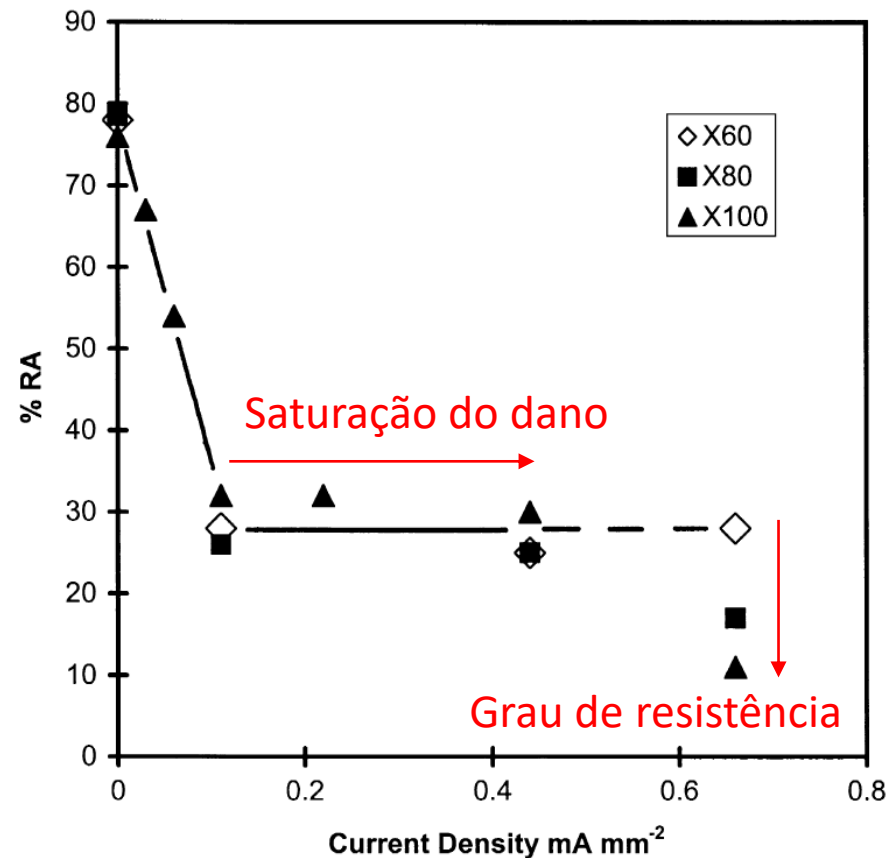
Literatura



Fonte: <https://doi.org/10.1515/corrrev-2022-0052>

Type	Experiment	Standards	Number of studies
Tensile	Slow strain rate tensile (SSRT)	ASTM G142, ASTM G129	30
	Small punch (SP)	ASTM E3205	2
	Tensile test	ASTM G142, ASTM E8	28
	Permeation	Devanathan-Stachurski method	34
Fatigue	Beam specimen		2
	Compact tension (CT)	ASTM E647	19
	Edge notched tension		2
	Eccentrically loaded single-edge notched tension (ESET)		3
	Spiral notch torsion test (SNTT)		1
	Wedge open loading (WOL)	ISO 7539	1
	Modified wedge open loading (MWOL)		1
	Circumferentially notched tension (CRT)	ASTM G142	9
	Compact tension (CT)	ASTM E647	2
	Hollow circumferentially notched tension		1
Fracture toughness	Three point bending (TPB)/Single-edge notched bending (SENB)	ASTM E1820	7
	Single-edge notch tension (SENT)		5
	Charpy pendulum impact test	ASTM E23	7
	Distribution		2
	Hydrogen microprint technique		2
	SCC		24
	Hydrogen-induced cracking	NACE TM0284	1
	U-bend test	ASTM G30	11
	Electrochemical impedance spectroscopy (EIS)	ASTM G106	18
	Potentiodynamic polarisation	ASTM G61	2
Impact	Scanning vibrating electron technique (SVET)		6
	Thermal desorption spectroscopy (TDS)		10
	Displacement methods		2
	Hydrogen analyser		2
	Hot extraction method		2
	Potentiometer		4
	discharging		2
	Disc pressure test		2
	Other		2

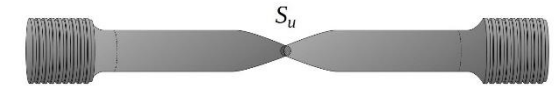
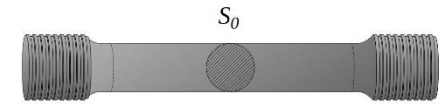
Literatura



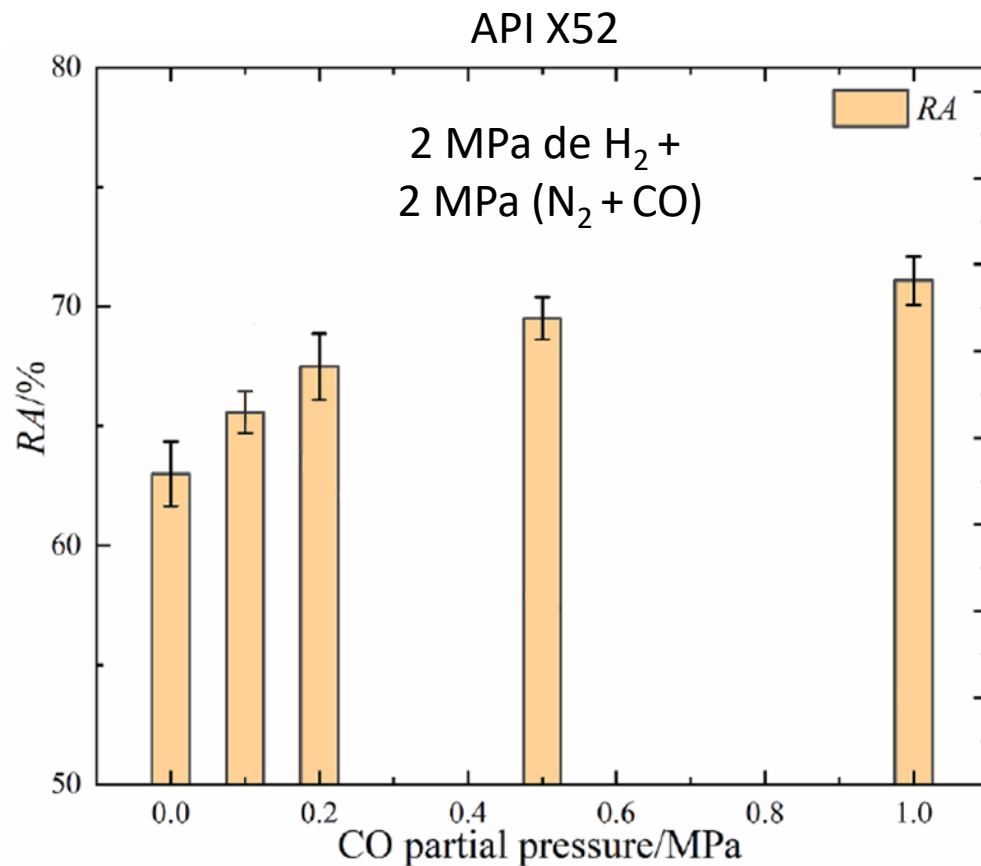
Steel	Current density mA mm ⁻²	% Reduction in area
X60	0	78
X60	0.11	28
X60	0.44	25
X60	0.66	28
X80	0	78
X80	0.11	26
X80	0.44	25
X80	0.66	17
X100	0	76
X100	0.03	67
X100	0.06	54
X100	0.11	32
X100	0.22	32
X100	0.44	30
X100	0.66	11
X100^a	0.66	77

^a Left one week in air at room temperature before straining.

Reversibilidade do
dano



Literatura



Fonte: adaptado de <https://doi.org/10.1016/j.engfailanal.2024.108111>.

Adsorção preferencial de CO na superfície do aço “atrapalha” ingresso de H.

O_2 e SO_2 também atuam nesse sentido enquanto H_2S favorece o dano.

CO_2 : resultados variados.

CH_4 e N_2 : sem efeito.

[1-3]

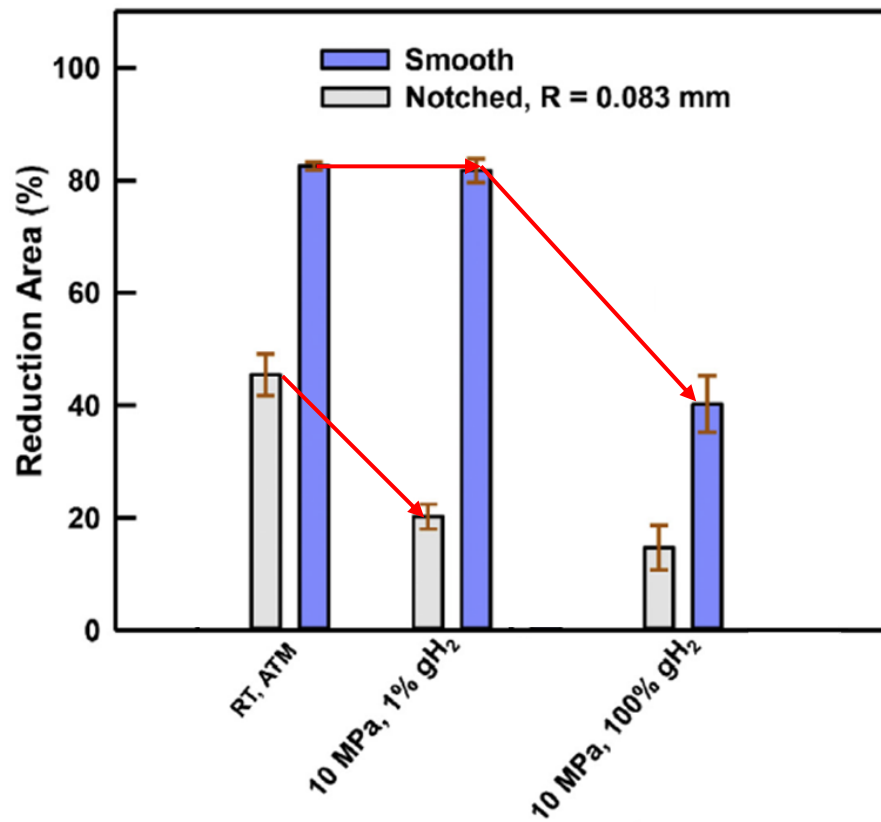
[1] Gallon, N. HYDROGEN PIPELINES – DESIGN AND MATERIAL CHALLENGES AND MITIGATIONS.

[2] <https://doi.org/10.1016/j.engfailanal.2024.108111>.

[3] <https://doi.org/10.1533/9780857093899.3.526>

Literatura

API X70
Misturas de CH₄ e H₂



Fonte: <https://doi.org/10.1016/j.ijhydene.2019.11.013>.

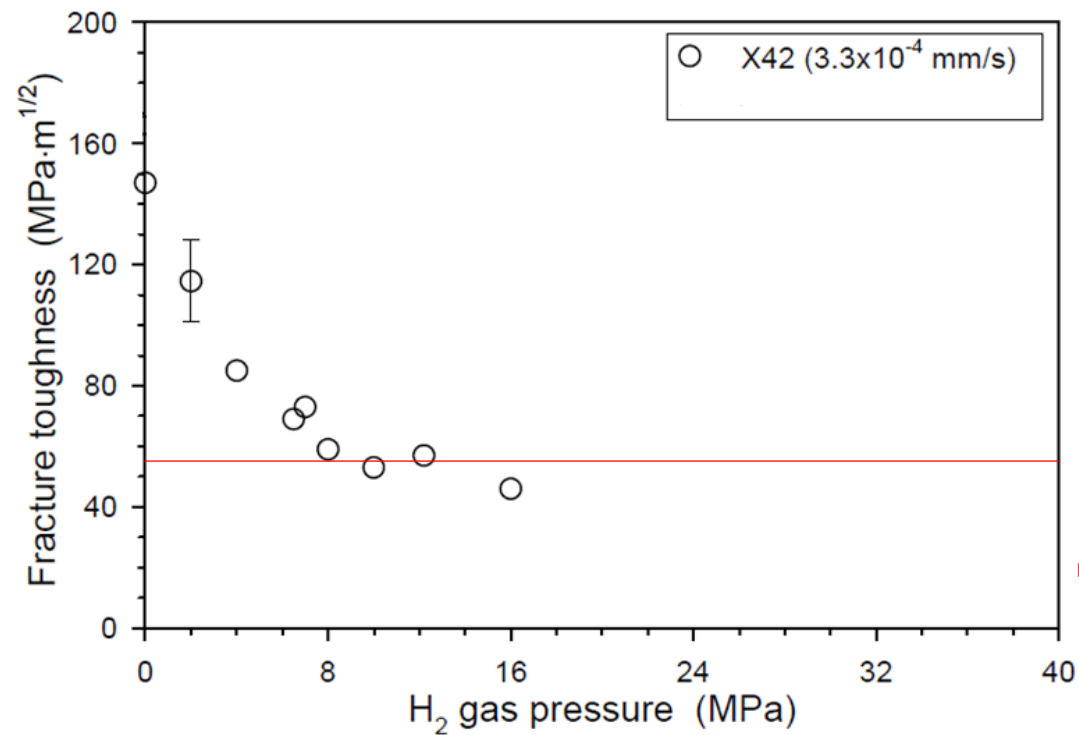


Smooth



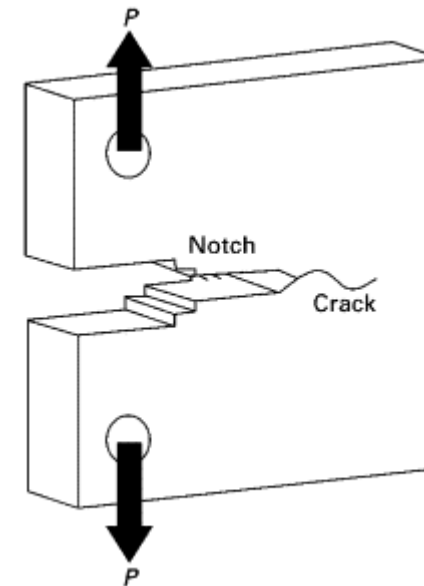
Notched

Literatura



55 MPa√m

Valor mínimo
requerido por um
critério da ASME
B31.12



Fonte: San Marchi, C. and Somerday, B.P. Sandia Report SAND2012-7321, Technical Reference for Hydrogen Compatibility of Materials. Albuquerque, NM : Sandia National Laboratories, 2012.

Literatura

Necessidade de estudos focados em:

- Soldas e zonas afetadas pelo calor [1]
- Criar uma base de dados confiável, explorando altas pressões de hidrogênio (100 MPa), especialmente para tenacidade à fratura e fadiga [2,3]

[1] <https://doi.org/10.1515/correv-2022-0052>

[2] <https://doi.org/10.1016/j.engfailanal.2024.108917>

[3] <https://doi.org/10.1533/9780857093899.3.526>

No IPT

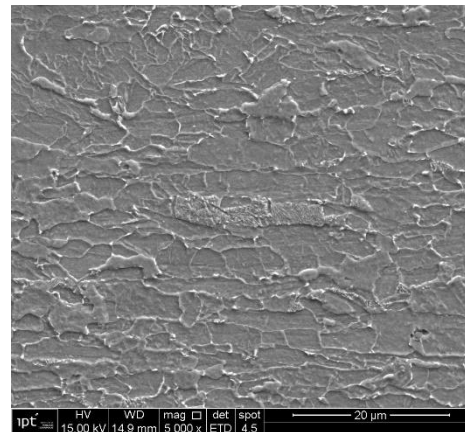
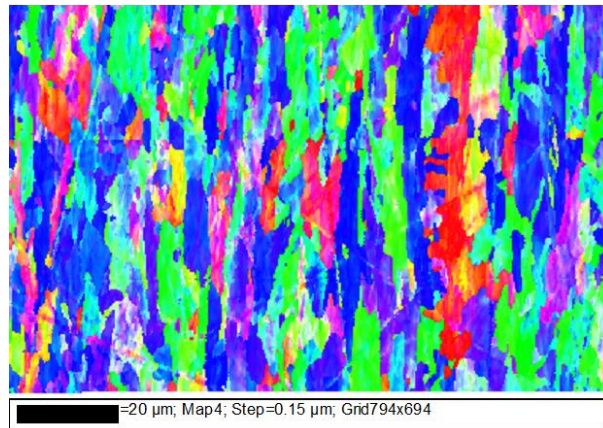


Tabela 01- Determinação elementares via SPARK OES (% massa)

Item	Identificação	Replicatas	C	S	Al	Si	P	Ti	V	Cr	Mn	Co	Ni	Cu
476/24	API X65	1	0,092	0,0080	0,035	0,233	0,0218	0,027	0,045	0,014	1,575	0,003	0,007	0,012
		2	0,085	0,0085	0,035	0,227	0,0216	0,028	0,045	0,012	1,567	0,003	0,007	0,012
		3	0,082	0,0085	0,032	0,227	0,0214	0,027	0,044	0,012	1,555	0,003	0,007	0,012
		Média	0,086	0,0083	0,034	0,229	0,0216	0,027	0,045	0,013	1,566	0,003	0,007	0,012
		Incerteza*	0,012	0,0007	0,004	0,008	0,0005	0,002	0,001	0,003	0,025	0,000	0,001	0,001

*A incerteza associada refere-se ao intervalo de confiança de 95%, utilizando a distribuição t de Student para n= 3

Aço API X65M

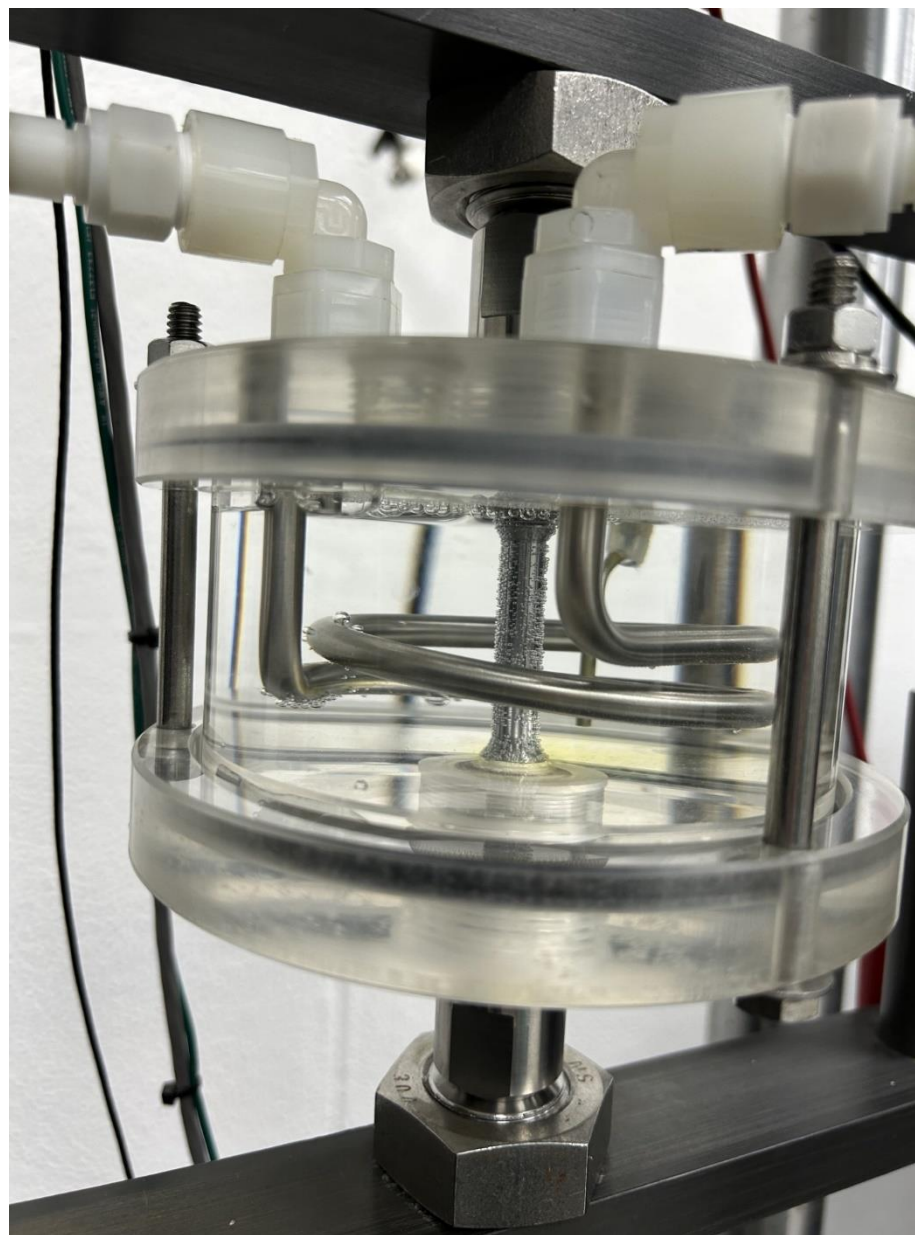
No IPT

7,8 MPa
40°C
24 h

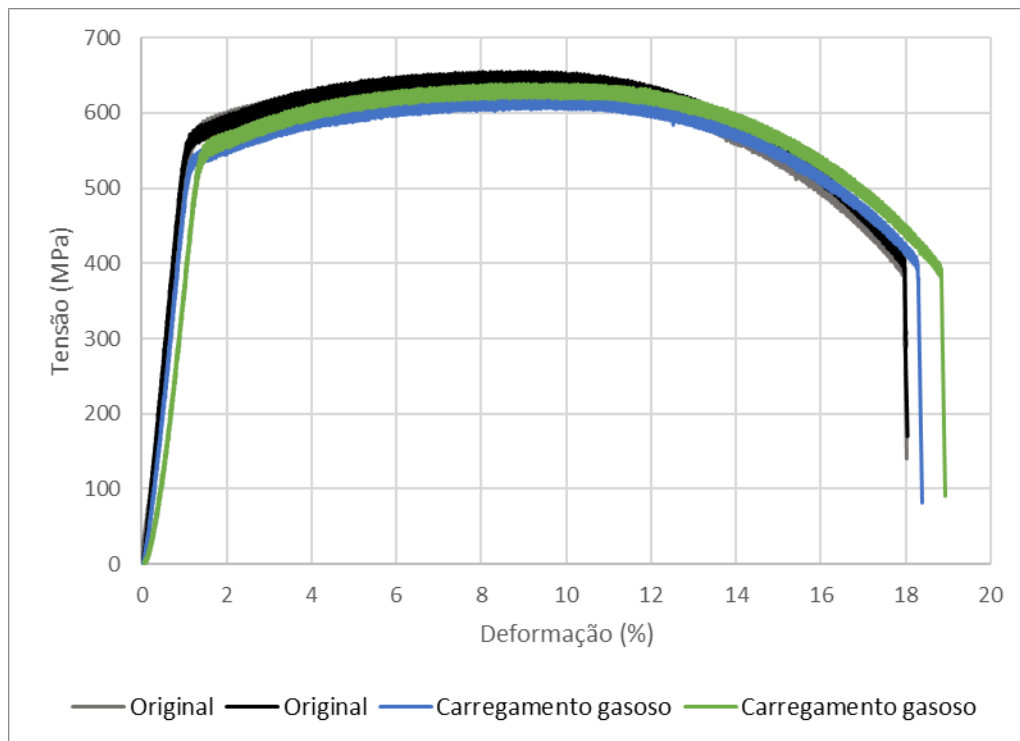
H₂ industrial
(até 10 ppm H₂O
e 10 ppm de O₂)



Carregamento gasoso



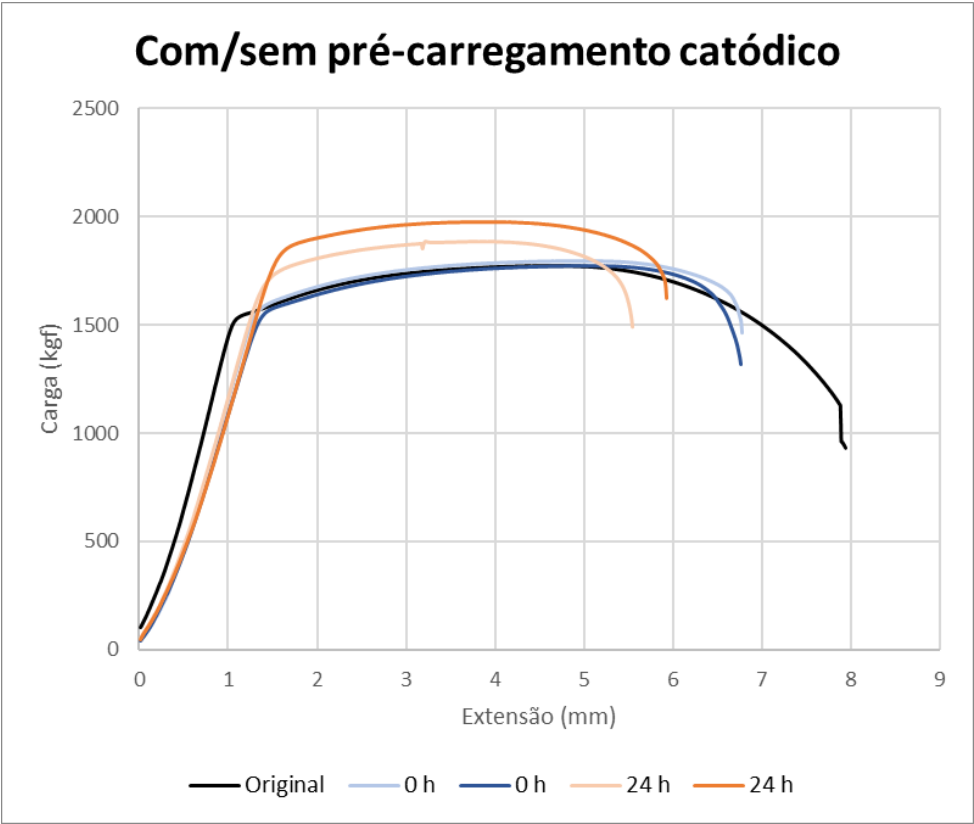
No IPT



	Original	Carregamento gasoso
LE 0,2% (MPa)	568 ± 6	538 ± 11
LR (MPa)	647 ± 11	631 ± 12
Alongamento (%)	18 ± 0	19 ± 0
Redução de área (%)	71 ± 2	66 ± 1

Sem diferenças para nível de confiança de 95%

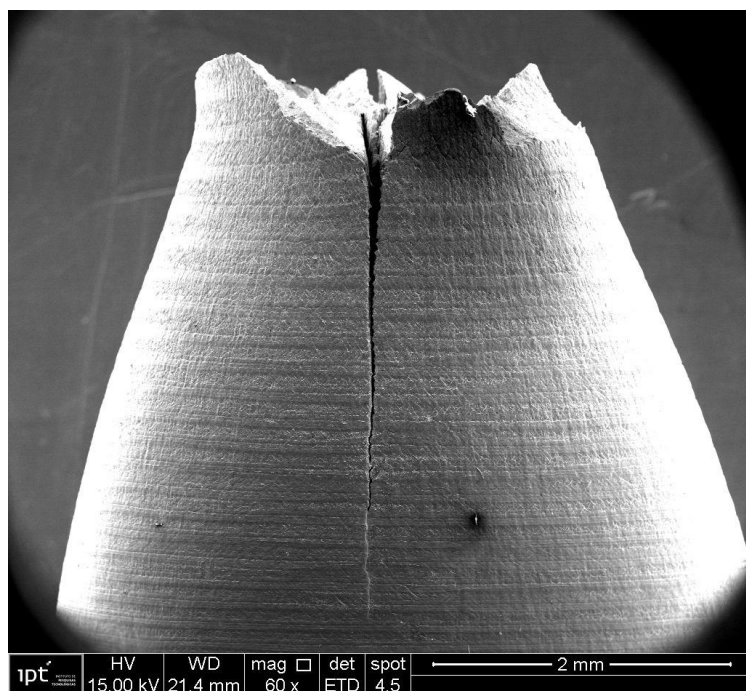
No IPT



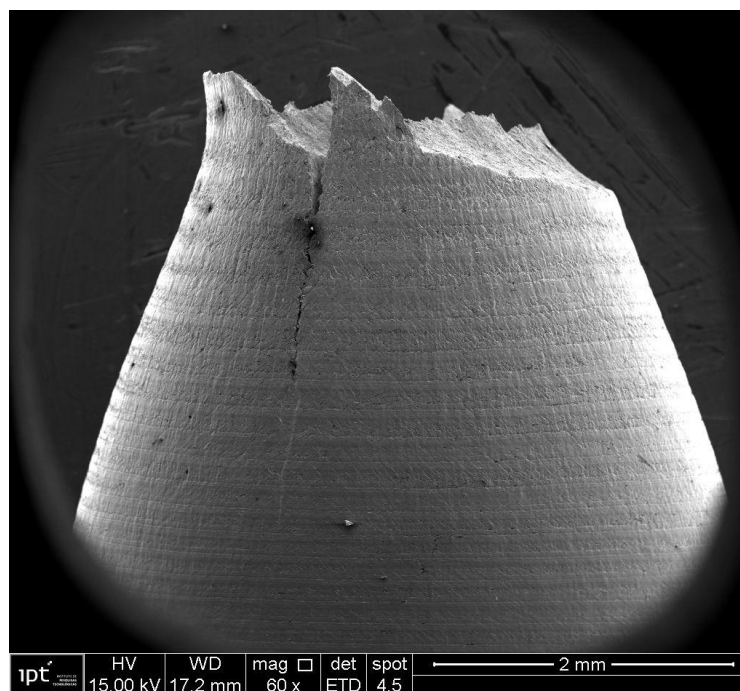
	Original	0 h	24 h
LR (kgf)	1776	1787 ± 15	1929 ± 64
Extensão (mm)	8	7 ± 0	6 ± 0
Redução de área (%)	74	34 ± 2	24 ± 4

Sem diferenças para nível de confiança de 95%

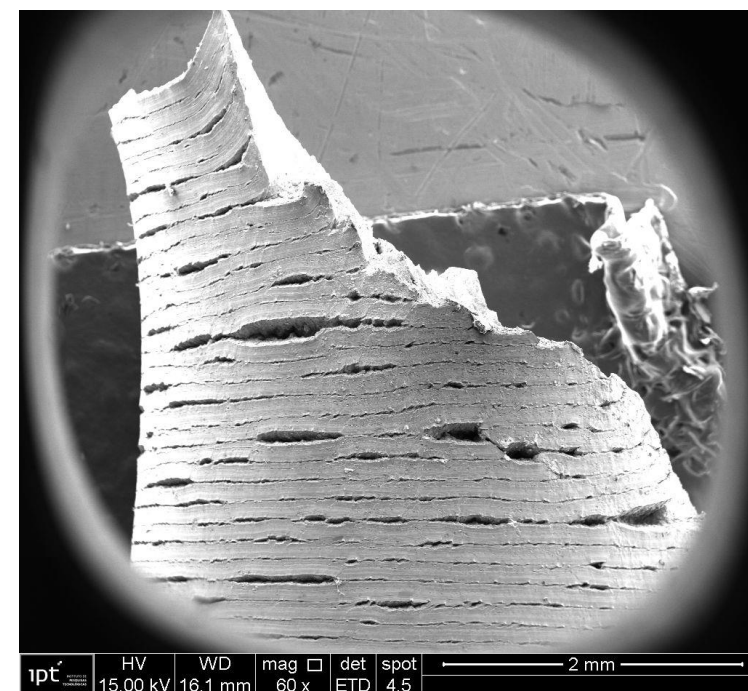
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Original

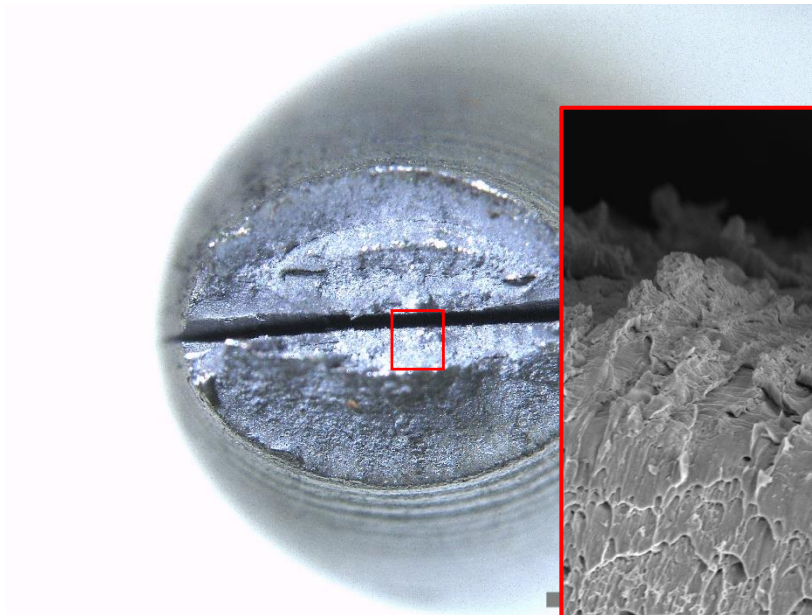


Carregamento gasoso

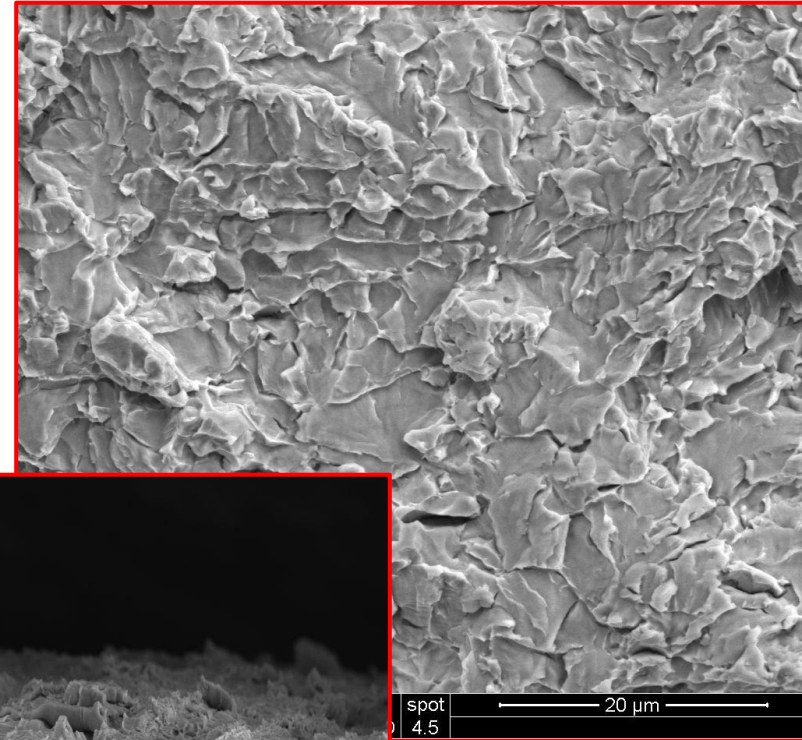
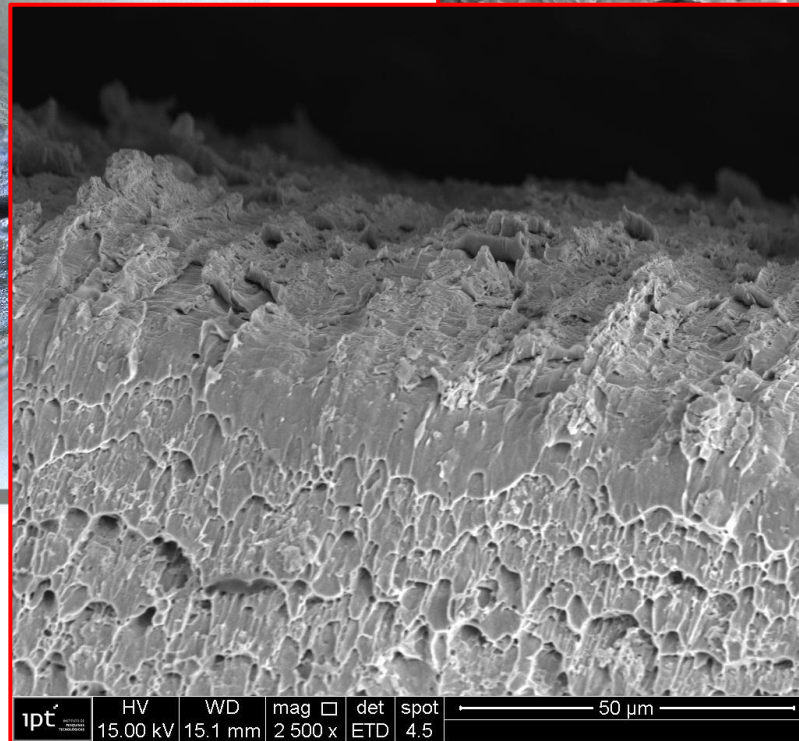


Carregamento catódico (0 h pré-carregamento)

No IPT



Original



tódico (0 h pré-carregamento)

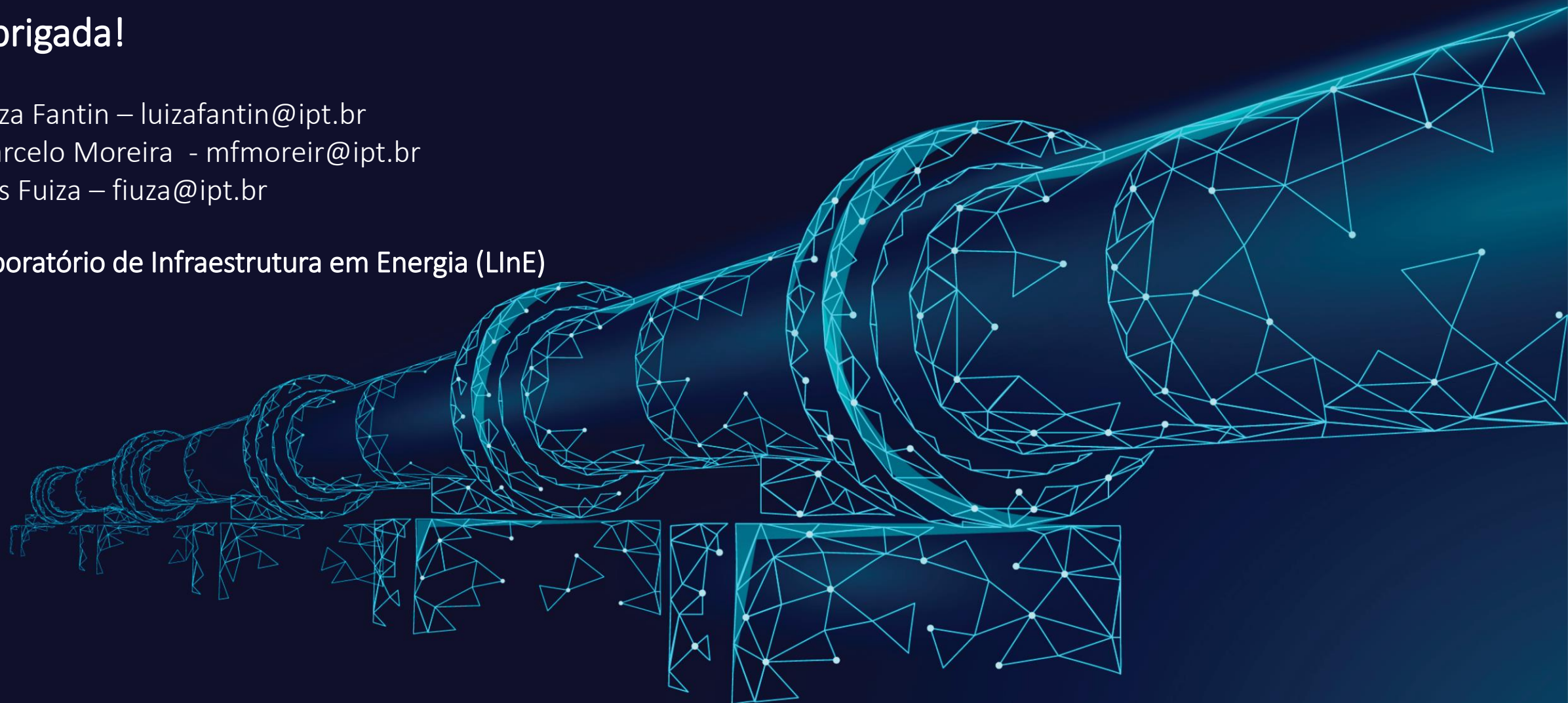
Obrigada!

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